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REPORT 3(U) COASTAL ENGINEERING RESEARCH CENTER
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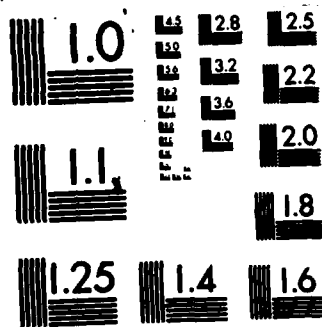
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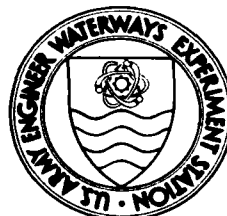
HANDHELD CALCULATOR ALGORITHMS FOR COASTAL ENGINEERING

Report 3

by

Julie L. Dean, Todd L. Walton, Jr.

Coastal Engineering Research Center
U. S. Army Engineer Waterways Experiment Station
P. O. Box 631, Vicksburg, Miss. 39180



December 1983

Report 3 of a Series

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Prepared for Office, Chief of Engineers, U. S. Army
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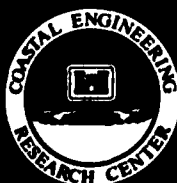
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| REPORT DOCUMENTATION PAGE | | READ INSTRUCTIONS BEFORE COMPLETING FORM |
|---|-------------------------------------|--|
| 1. REPORT NUMBER Miscellaneous Paper CERC-83-9 | 2. GOVT ACCESSION NO. AD-A138369 | 3. RECIPIENT'S CATALOG NUMBER |
| 4. TITLE (and Subtitle) HANDHELD CALCULATOR ALGORITHMS FOR COASTAL ENGINEERING: Report 3 | | 5. TYPE OF REPORT & PERIOD COVERED Report 3 of a series |
| | | 6. PERFORMING ORG. REPORT NUMBER |
| 7. AUTHOR(s) Julie L. Dean and Todd L. Walton, Jr. | | 8. CONTRACT OR GRANT NUMBER(s) |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS U. S. Army Engineer Waterways Experiment Station Coastal Engineering Research Center P. O. Box 631, Vicksburg, Miss. 39180 | | 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS |
| 11. CONTROLLING OFFICE NAME AND ADDRESS Office, Chief of Engineers, U. S. Army Washington, D. C. 20314 | | 12. REPORT DATE December 1983 |
| | | 13. NUMBER OF PAGES 29 |
| 14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) | | 15. SECURITY CLASS. (of this report) Unclassified |
| | | 15a. DECLASSIFICATION/DOWNGRADING SCHEDULE |
| 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. | | |
| 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) | | |
| 18. SUPPLEMENTARY NOTES Available from National Technical Information Service, 5285 Port Royal Road, Springfield, Va. 22161. | | |
| 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Calculator algorithm Significant wave height Coastal engineering Spectral wave height Peak spectral period | | |
| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) > This is the third in a series of reports providing handheld calculator algorithms for use in coastal engineering. The first and second reports in this series were published as Coastal Engineering Technical Aids (CETA's) and are available from the U. S. Army Engineer Waterways Experiment Station Tech- nical Report Distribution Center, Vicksburg, Miss. Of these, CETA 82-1 pre- sents a set of six algorithms for programs useful in performing certain wave (Continued) | | |

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20. ABSTRACT (Continued).

transformation and wave generation calculations with both the Texas Instruments TI-59 (Algebraic Operating System (AOS) notation) and the Hewlett-Packard HP-67 (Reverse Polish Notation (RPN)); CETA 82-4 presents the same six algorithms for use on the HP-41CV (RPN).

The present report provides algorithms for three calculator programs that forecast gravity water waves in deep and shallow water. Two programs use the Joint North Sea Wave Project (JONSWAP) shallow- and deepwater wave forecasting equations as presented in the Coastal Engineering Research Center's Shore Protection Manual (revised edition to be published in 1984). The third program uses equations to predict a depth-limited significant wave height. The programs are intended for use with the HP-41CV.

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PREFACE

This report was prepared as part of the Littoral Data Collection Methods and Their Engineering Application Research Work Unit, Shore Protection and Restoration Program, Coastal Engineering Area of Civil Works Research and Development. Technical Monitors from the Office, Chief of Engineers for the Coastal Engineering Area are Mr. John H. Lockhart, Jr., and Mr. John Housley.

This work was accomplished during the period 1 July 1983 through 30 December 1983 by The Coastal Engineering Research Center (CERC) of the U. S. Army Engineer Waterways Experiment Station (WES), under the general supervision of Dr. Robert W. Whalin, Chief, CERC; Dr. Lewis E. Link, Assistant Chief, CERC; Dr. Dennis R. Smith and Mr. Fred E. Canfield, Acting Chiefs, Engineering Development Division; and Mr. Thomas W. Richardson, Chief, Coastal Structures and Evaluation Branch. This report was prepared by Ms. Julie L. Dean, Engineering Assistant, and Dr. Todd L. Walton, Jr., Research Hydraulic Engineer.

Commander and Director of WES during the publication of this report was COL Tilford C. Creel, CE. Mr. F. R. Brown was Technical Director.

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CONVERSION FACTORS, INCH-POUND TO METRIC (SI)
UNITS OF MEASUREMENTS

Inch-pound units of measurement used in this report have been converted to metric (SI) units as follows:

| <u>Multiply</u> | <u>By</u> | <u>To Obtain</u> |
|-----------------------------------|-----------|-------------------|
| feet | 0.3048 | meters |
| miles (U. S. statute) | 1.609347 | kilometers |
| miles per hour (international) | 0.44704 | meters per second |

HANDHELD CALCULATOR ALGORITHMS FOR COASTAL ENGINEERING

Report 3

PART I: INTRODUCTION

1. The advent of the handheld programmable calculator has led to the development of numerous programs in various fields of engineering and science. Coastal engineering is no exception. This report provides three programs to forecast waves in deep and shallow water. Two programs use the Joint North Sea Wave Project (JONSWAP) wave forecasting equations for deep and shallow water as presented in the Shore Protection Manual (U. S. Army Engineer Waterways Experiment Station Coastal Engineering Research Center (CERC), in preparation, 1984). The third program predicts a depth-limited significant wave height using a spectral approach (Vincent 1982, Thompson and Vincent 1983).

2. The three programs presented herein are versions of Reverse Polish Notation (RPN) logic suitable for use on HP-41CV programmable calculators with or without accessory printer. Each program is documented, assumptions are briefly described, and references to more detailed presentations of the theory are given.

3. Each of the RPN programs incorporates HP-41 compatible-print routines which print and label all input and output parameters. The user has only to enter the input parameters and the results are automatically computed and printed. Since the printing routines increase program length by as much as 25 percent, use of a magnetic card for permanent program storage is recommended. The print steps do not need to be deleted if a printer is unavailable.

PART II: PROGRAMS

4. Three programs (103R-Rev, 106R, and 107R) are presented in this report. Program 103R-Rev is a revised version of Program 103R (Walton, Birkemeier, and Weggel 1982) and is being published herein with slight changes for consistency.

5. Program 103R-Rev forecasts significant wave height and spectral peak period in shallow water, using JONSWAP wave forecasting equations of the Shore Protection Manual (CERC, in preparation, 1984). Program 106R forecasts the deepwater significant wave height and spectral peak period for fetch-limited, duration-limited, and fully developed sea cases in deep water. The JONSWAP forecasting equations used are presented in Table 3-2 of the Shore Protection Manual (CERC, in preparation, 1984). Program 107R calculates a depth-limited significant wave height based on an estimate of the peak frequency of shallow-water storm wave spectra. Equation (14) from Vincent (1982) and equation (5) from Thompson and Vincent (1983) are used.

6. Each program allows either English or metric input and output. Program listings are annotated, making it possible to follow the logic of the algorithm and to make modifications if desired.

7. There are undoubtedly many calculator programs not included here that have been developed on coastal engineering subjects. Practicing engineers who would like to share such programs (in either AOS or RPN) with other users are encouraged to submit them to the CERC. If the response is great enough, additional reports presenting the programs will be prepared. Comments, programs, or suggestions for programs should be sent to:

Commander and Director
U. S. Army Engineer Waterways Experiment Station
ATTN: Coastal Structures and Evaluation Branch, CERC
P. O. Box 631
Vicksburg, Mississippi 39180

8. These and future programs will generally correspond to the following numbering scheme:

| | | | |
|--------------------|---------|------------|----------|
| Miscellaneous | 0-99 | Beaches | 500-699 |
| Waves and currents | 100-299 | Geology | 700-899 |
| Inlets | 300-499 | Structures | 900-1099 |

9. In general, the documentation of programs submitted should be in a format paralleling that of the programs presented in this report. A blank set of forms which can be reproduced is included in Appendix A

Program Description

| | | | |
|----------------------|--|-----------------|-------|
| Program Title | 103R-41CV-REV: JONSWAP Shallow-Water Wave Forecasting Equations, Revised (RPN Logic) | | |
| Name | Todd L. Walton, Jr. | Date | 7/83 |
| Address | Coastal Engineering Research Center | | |
| City | Waterways Experiment Station | State | MS |
| | Vicksburg | Zip Code | 39180 |

Program Description, Equations, Variables, etc.

This algorithm computes the wave height, H , wave period, T , and minimum duration, t , from input values of the water depth, d , fetch length, F , and adjusted windspeed, U_A using equations (3-39), (3-40), and (3-41) of the Shore Protection Manual (CERC, in preparation, 1984). Equations (3-39) and 3-40) are for constant depth and unlimited wind duration. Wave height and period in this algorithm are significant wave height and period. Algorithm uses English or metric system of units.

REFERENCE

U. S. Army Engineers, Coastal Engineering Research Center, Shore Protection Manual, Chapter 3 (in preparation).

Operating Limits and Warnings

103R-41CV-REV.-1

User Instructions

103R-41CV-REV: JONSWAP Shallow-Water Wave Forecasting
Equations, Revised (RPN Logic)

SIZE: 010

| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
|-------------------------|--|----------------|-------------------------------------|------------------|
| 1 | LOAD PROGRAM (FOCAST) | | [XEQ]"FOCAST" | E OR M? |
| 2 | CHOOSE ENGLISH OR METRIC UNITS | | E or M, [R/S] | U _A ? |
| 3 | ENTER ADJUSTED WINDSPEED (miles per hour or meters per sec) | U _A | [R/S] | FETCH? |
| 4 | ENTER FETCH (feet or km) | F | [R/S] | DEPTH? |
| 5 | ENTER DEPTH (feet or m) | d | [R/S] | |
| 6 | READ SIGNIFICANT WAVE HEIGHT (feet or meters) | | | H |
| 7 | READ SIGNIFICANT WAVE PERIOD (sec) | | | T |
| 8 | READ MINIMUM DURATION (hours) | | | TIME |
| <u>Example Problem:</u> | | | | |
| | U _A = 50 mph = 22 m/sec | | | |
| | F = 80,000 ft. = 24.4 km | | | |
| | d = 35 ft. = 11 m. | | | |
| | SHALLOW FORECASTING ENGLISH UNITS | | SHALLOW FORECASTING METRIC UNITS | |
| | U _A = 50.0000 *** | | U _A = 22.0000 *** | |
| | FETCH = 80,000.0000 *** | | FETCH = 24.4000 *** | |
| | DEPTH = 35.0000 *** | | DEPTH = 11.0000 *** | |
| | H = 4.9790 | | H = 1.4930 | |
| | T = 4.4100 | | T = 4.4044 | |
| | TIME = 1.5800 | | TIME = 1.6155 | |

103R-41CV-REV.-2

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|-----------------|----------|---|------|-----------|----------|--|
| 01 | LBL "FOCAL" | | | 60 | * | | |
| 02 | "SHALLOW FOCAL" | | | 61 | STO 07 | | $U_A \text{ converted} \rightarrow R_{07}$ |
| 03 | "-TING" | | | 62 | PCL 09 | | |
| 04 | AVIEW | | | 63 | PCL 07 | | |
| 05 | LBL 05 | | | 64 | Y+2 | | |
| 06 | "E OR M?" | | | 65 | / | | $g/U_A^2 \rightarrow R_{00}$ |
| 07 | 000 | | | 66 | STO 08 | | |
| 08 | TONE 1 | | | 67 | PCL 06 | | |
| 09 | PROMPT | | | 68 | * | | $g^2/U_A^2 \rightarrow R_{00}$ |
| 10 | ROFF | | | 69 | STO 00 | | |
| 11 | ASTO Y | | | 70 | PCL 03 | | |
| 12 | CLA | | | 71 | PCL 01 | | |
| 13 | "M" | | | 72 | * | | |
| 14 | ASTO X | | | 73 | PCL 05 | | |
| 15 | CLA | | | 74 | * | | $gF/U_A^2 \rightarrow R_{01}$ |
| 16 | X=Y | | | 75 | STO 01 | | |
| 17 | GTO 01 | | | 76 | PCL 00 | | |
| 18 | "ENGLISH UNITS" | | | 77 | .75 | | |
| 19 | AVIEW | | | 78 | Y+X | | |
| 20 | 32.2 | | | 79 | .53 | | |
| 21 | STO 09 | | $g_{\text{English}} \rightarrow R_{09}$ | 80 | * | | |
| 22 | 1.47 | | | 81 | XEQ 03 | | |
| 23 | STO 07 | | Eng. Conversion $\rightarrow R_{01}$ | 82 | STO 04 | | $\tanh[0.53(g/U_A^2)^{.75}] \rightarrow R_{01}$ |
| 24 | 1.0 | | | 83 | PCL 01 | | |
| 25 | STO 01 | | Eng. Conversion $\rightarrow R_{01}$ | 84 | SORT | | |
| 26 | GTO 02 | | | 85 | .00565 | | |
| 27 | LBL 01 | | | 86 | * | | |
| 28 | "METRIC UNITS" | | | 87 | PCL 04 | | |
| 29 | AVIEW | | | 88 | / | | $\tanh\left[\frac{0.00565(gF/U_A^2)^{.75}}{R_{04}}\right]$ |
| 30 | 9.81 | | | 89 | XEQ 03 | | |
| 31 | STO 09 | | $g_{\text{Metric}} \rightarrow R_{09}$ | 90 | PCL 04 | | |
| 32 | 1.0 | | | 91 | * | | |
| 33 | STO 07 | | Metric Conversion $\rightarrow R_{01}$ | 92 | .283 | | |
| 34 | 1000 | | | 93 | * | | |
| 35 | STO 01 | | Metric Conversion $\rightarrow R_{01}$ | 94 | PCL 08 | | |
| 36 | LBL 02 | | | 95 | / | | |
| 37 | "U?" | | | 96 | "H=" | | H displayed. |
| 38 | TONE 2 | | | 97 | ARCL X | | |
| 39 | PROMPT | | | 98 | AVIEW | | |
| 40 | "U?" | | | 99 | TONE 7 | | |
| 41 | FS? 55 | | | 100 | PCL 00 | | |
| 42 | XEQ 04 | | | 101 | .375 | | |
| 43 | STO 03 | | $U_A \rightarrow R_{03}$ | 102 | Y+X | | |
| 44 | "FETCH?" | | | 103 | .833 | | |
| 45 | TONE 3 | | | 104 | * | | |
| 46 | PROMPT | | | 105 | XEQ 03 | | $\tanh[0.833(g/U_A^2)^{.833}] \rightarrow R_{04}$ |
| 47 | "FETCH=" | | | 106 | STO 04 | | |
| 48 | FS? 55 | | | 107 | PCL 01 | | |
| 49 | XEQ 04 | | | 108 | .333 | | |
| 50 | STO 05 | | $F \rightarrow R_{05}$ | 109 | Y+X | | |
| 51 | "DEPTH?" | | | 110 | .0379 | | |
| 52 | TONE 4 | | | 111 | * | | |
| 53 | PROMPT | | | 112 | PCL 04 | | |
| 54 | "DEPTH=" | | | 113 | / | | $\tanh\left[\frac{0.0379(gF/U_A^2)^{.833}}{R_{04}}\right]$ |
| 55 | FS? 55 | | | 114 | XEQ 03 | | |
| 56 | XEQ 04 | | | 115 | PCL 04 | | |
| 57 | STO 06 | | $d \rightarrow R_{06}$ | 116 | * | | |
| 58 | PCL 03 | | | 117 | 7.54 | | |
| 59 | PCL 07 | | | 118 | * | | |

103R-41CV-REV.-3

[illegible]

Program Description

| | | | |
|----------------------|---|-----------------|-------|
| Program Title | 106R-41CV: JONSWAP Deepwater Wave Forecasting Equations (RPN Logic) | | |
| Name | Julie L. Dean | Date | 7/83 |
| Address | Coastal Engineering Research Center | | |
| City | Vicksburg | State | MS |
| | | Zip Code | 39180 |

Program Description, Equations, Variables, etc.

This program takes the fetch length, F , adjusted windspeed, U_A , and duration, t , as input values and calculates the deepwater spectral wave height, H_{MO} , and the peak spectral period, T_m , for fetch-limited, duration-limited, and fully developed sea cases in deep water. The equations used are presented in the Shore Protection Manual, Table 3-20. The algorithm uses either English or metric units.

REFERENCE

U. S. Army Engineer Waterways Experiment Station, Shore Protection Manual, Chapter 3 (in preparation).

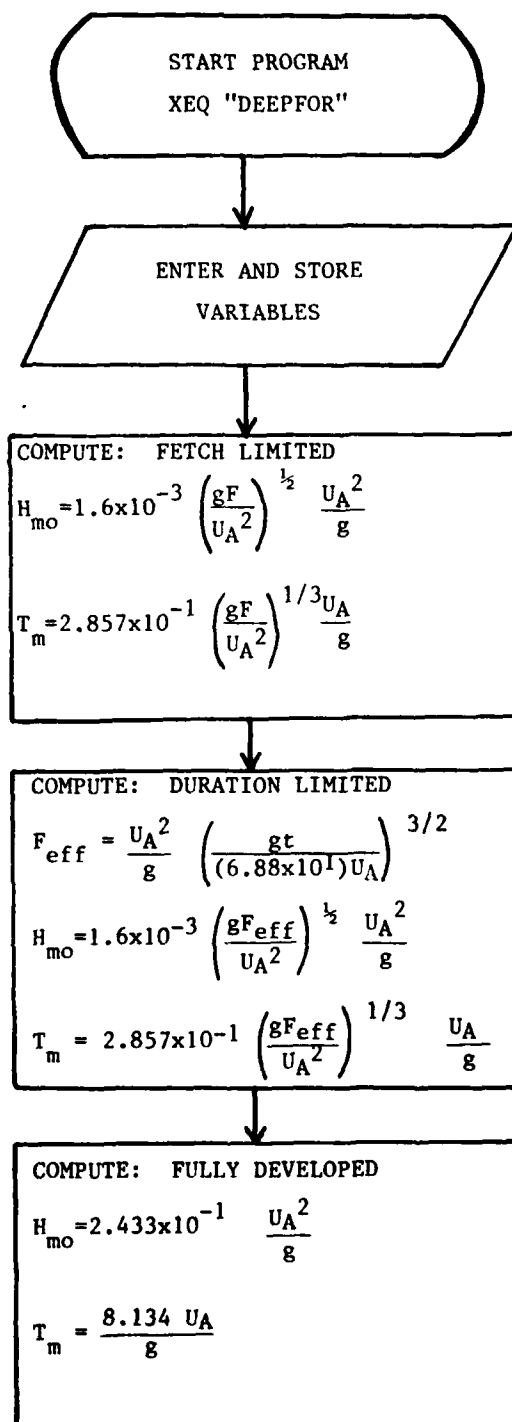
Operating Limits and Warnings

106R-41CV-1

106R-41CV: JONSWAP Deepwater Wave Forecasting
Equations (RPN Logic)

| 106R-41CV: JONSWAP Deepwater Wave Forecasting Equations (RPN Logic) | | | | SIZE: 010 |
|--|--|---|-----------------|---|
| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
| 1 | LOAD PROGRAM (DEEPPOR) | | [XEQ] "DEEPPOR" | E OR M? |
| 2 | CHOOSE ENGLISH OR METRIC UNITS | | E or M, [R/S] | FETCH? |
| 3 | ENTER FETCH (miles or kilometers) | F | [R/S] | UA? |
| 4 | ENTER ADJUSTED WINDSPEED (miles/hr or meters/sec) | UA | [R/S] | DURATION? |
| 5 | ENTER DURATION (hours) | t | [R/S] | |
| 6 | FETCH-LIMITED CASE | | | |
| | READ H _{MO} , SPECTRAL WAVE HT. | | | H _{MO} (ft. or m.) |
| | READ T _M , PEAK SPECTRAL PERIOD | | | T _M (SEC.) |
| 7 | DURATION-LIMITED CASE | | | |
| | READ H _{MO} , SPECTRAL WAVE HT. | | | H _{MO} (ft. or m.) |
| | READ T _M , PEAK SPECTRAL PERIOD | | | T _M (SEC.) |
| 8 | FULLY DEVELOPED CASE | | | |
| | READ H _{MO} , SPECTRAL WAVE HT. | | | H _{MO} (ft. or m.) |
| | READ T _M , PEAK SPECTRAL PERIOD | | | T _M (SEC.) |
| 9 | PRESS R/S TO ENTER A NEW PROBLEM | | | |
| <p><u>Example Problem:</u></p> <p>F = 9.21 miles = 14.83 km</p> <p>UA = 46.05 miles/hr. = 20.59 meters/sec</p> <p>t = 20 hours</p> | | | | |
| | | DEEPPOR FORECASTING ENGLISH UNITS FETCH= 9.2100 *** UA= 46.0500 *** DURATION= 20.0000 *** | | DEEPPOR FORECASTING METRIC UNITS FETCH= 14.8300 * UA= 20.5900 * DURATION= 20.0000 * |
| | | FETCH LIMITED HMO=4.2065 TM=4.1999 | | FETCH LIMITED HMO=1.2814 TM=4.2006 |
| | | DURATION LIMITED HMO=23.9700 TM=12.3986 | | DURATION LIMITED HMO=7.2964 TM=13.3953 |
| | | FULLY DEVELOPED HMO=34.4596 TM=17.0661 | | FULLY DEVELOPED HMO=10.5228 TM=17.0697 |
| | | | | 106R-41CV-2 |

PROGRAM DEEPFOR FLOWCHART



Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|-------------------|----------|--|------|-------------------|----------|--------------------------|
| 01 | LBL "DEEPOF" | | | 59 | "H0=" | | |
| 02 | "DEEPWATER FOREC" | | | 60 | FS? 55 | | |
| 03 | "PASTING" | | | 61 | XEQ 03 | | |
| 04 | AVIEW | | | 62 | STO 02 | | $U_A \rightarrow R_{02}$ |
| 05 | LBL 04 | | | 63 | "DURATION?" | | |
| 06 | "E OR M?" | | | 64 | TONE 5 | | |
| 07 | ADV | | | 65 | PROMPT | | |
| 08 | TONE 2 | | | 66 | "DURATION=" | | |
| 09 | PROMPT | | | 67 | FS? 55 | | |
| 10 | AOFF | | | 68 | XEQ 03 | | |
| 11 | ASTO Y | | | 69 | STO 03 | | $t \rightarrow R_{03}$ |
| 12 | CLA | | | 70 | ADV | | |
| 13 | "M" | | | 71 | "FETCH LIMITED" | | |
| 14 | ASTO X | | | 72 | AVIEW | | |
| 15 | CLA | | | 73 | RCL 01 | | |
| 16 | X=Y? | | | 74 | SORT | | |
| 17 | GTO 01 | | | 75 | RCL 02 | | |
| 18 | "ENGLISH UNITS" | | | 76 | * | | |
| 19 | AVIEW | | | 77 | RCL 04 | | |
| 20 | 3.01 E-2 | | (English) $3.01 \times 10^{-2} = \frac{H_{MO}}{U_A F^5} \rightarrow R_{04}$ | 78 | * | | |
| 21 | STO 04 | | | 79 | "HMO=" | | |
| 22 | 5.59 E-1 | | $5.59 \times 10^{-1} = \frac{T_M}{(U_A F)^5} \rightarrow R_{05}$ | 80 | ARCL X | | |
| 23 | STO 05 | | | 81 | AVIEW | | |
| 24 | 2.1128 E-2 | | $2.1128 \times 10^{-2} = \frac{H_{MO}}{U_A^{1.25} t^{.75}} \rightarrow R_{06}$ | 82 | TONE 4 | | |
| 25 | STO 06 | | | 83 | RCL 02 | | |
| 26 | 4.415 E-1 | | $4.415 \times 10^{-1} = \frac{T_M}{U_A^5 t^5} \rightarrow R_{07}$ | 84 | RCL 01 | | |
| 27 | STO 07 | | | 85 | * | | |
| 28 | 1.625 E-2 | | $1.625 \times 10^{-2} = \frac{H_{MO}}{U_A^2} \rightarrow R_{08}$ | 86 | * | | |
| 29 | STO 08 | | | 87 | 1/X | | |
| 30 | 3.706 E-1 | | $3.706 \times 10^{-1} = \frac{T_M}{U_A} \rightarrow R_{09}$ | 88 | Y+X | | |
| 31 | STO 09 | | | 89 | RCL 05 | | |
| 32 | GTO 02 | | | 90 | * | | |
| 33 | LBL 01 | | | 91 | "TM=" | | |
| 34 | "METRIC UNITS" | | | 92 | APCL X | | |
| 35 | AVIEW | | (Metric) $1.616 \times 10^{-2} = \frac{H_{MO}}{U_A F^5} \rightarrow R_{04}$ | 93 | AVIEW | | |
| 36 | 1.616 E-2 | | | 94 | TONE 5 | | |
| 37 | STO 04 | | | 95 | ADV | | |
| 38 | 6.238 E-1 | | $6.238 \times 10^{-1} = \frac{T_M}{(U_A F)^5} \rightarrow R_{05}$ | 96 | "DURATION LIMITE" | | |
| 39 | STO 05 | | | 97 | "H0" | | |
| 40 | 1.759 E-2 | | $1.759 \times 10^{-2} = \frac{H_{MO}}{U_A^{1.25} t^{.75}} \rightarrow R_{06}$ | 98 | AVIEW | | |
| 41 | STO 06 | | | 99 | RCL 03 | | |
| 42 | 6.601 E-1 | | $6.601 \times 10^{-1} = \frac{T_M}{U_A^5 t^5} \rightarrow R_{07}$ | 100 | .75 | | |
| 43 | STO 07 | | | 101 | Y+X | | |
| 44 | 2.4821 E-2 | | $2.4821 \times 10^{-2} = \frac{H_{MO}}{U_A^2} \rightarrow R_{08}$ | 102 | RCL 02 | | |
| 45 | STO 08 | | | 103 | 1.25 | | |
| 46 | 9.3 E-1 | | $9.3 \times 10^{-1} = \frac{T_M}{U_A} \rightarrow R_{09}$ | 104 | Y+X | | |
| 47 | STO 09 | | | 105 | * | | |
| 48 | LBL 02 | | | 106 | RCL 06 | | |
| 49 | "FETCH?" | | | 107 | * | | |
| 50 | TONE 3 | | | 108 | "HMO=" | | |
| 51 | PROMPT | | | 109 | ARCL X | | |
| 52 | "FETCH=" | | | 110 | AVIEW | | |
| 53 | FS? 55 | | | 111 | TONE 6 | | |
| 54 | XEQ 03 | | | 112 | RCL 03 | | |
| 55 | STO 01 | | | 113 | RCL 02 | | |
| 56 | "H0?" | | | 114 | * | | |
| 57 | TONE 4 | | | 115 | SORT | | |
| 58 | PROMPT | | | 116 | RCL 07 | | |
| | | | $F \rightarrow R_{01}$ | | | | |

106R-41CV-4

Program Description

Program Title 107R-41CV: Depth-Limited Significant Wave Height (RPN Logic)

Name Julie L. Dean

Date 4/83

Address Coastal Engineering Research Center

City Vicksburg

State MS

Zip Code 39180

Program Description, Equations, Variables, etc.

This program calculates a depth-limited significant wave height as given by equation (14) from Vincent (1982) and equation (5) from Thompson and Vincent (1983), given depth, peak frequency of the wave spectrum, and Phillip's equilibrium coefficient. The low cut-off frequency is 0.80 fp. The upper cut-off frequency is 2.0 fp, where fp is the peak frequency. Simpson's Rule is used to numerically integrate the frequency spectrum. The algorithm uses either English or metric units.

REFERENCES

Vincent, C. L. 1982. "Depth-Limited Significant Wave Height: A Spectral Approach," Coastal Engineering Research Center Technical Report 82-3, U. S. Army Corps of Engineers Coastal Engineering Research Center, August 1982.

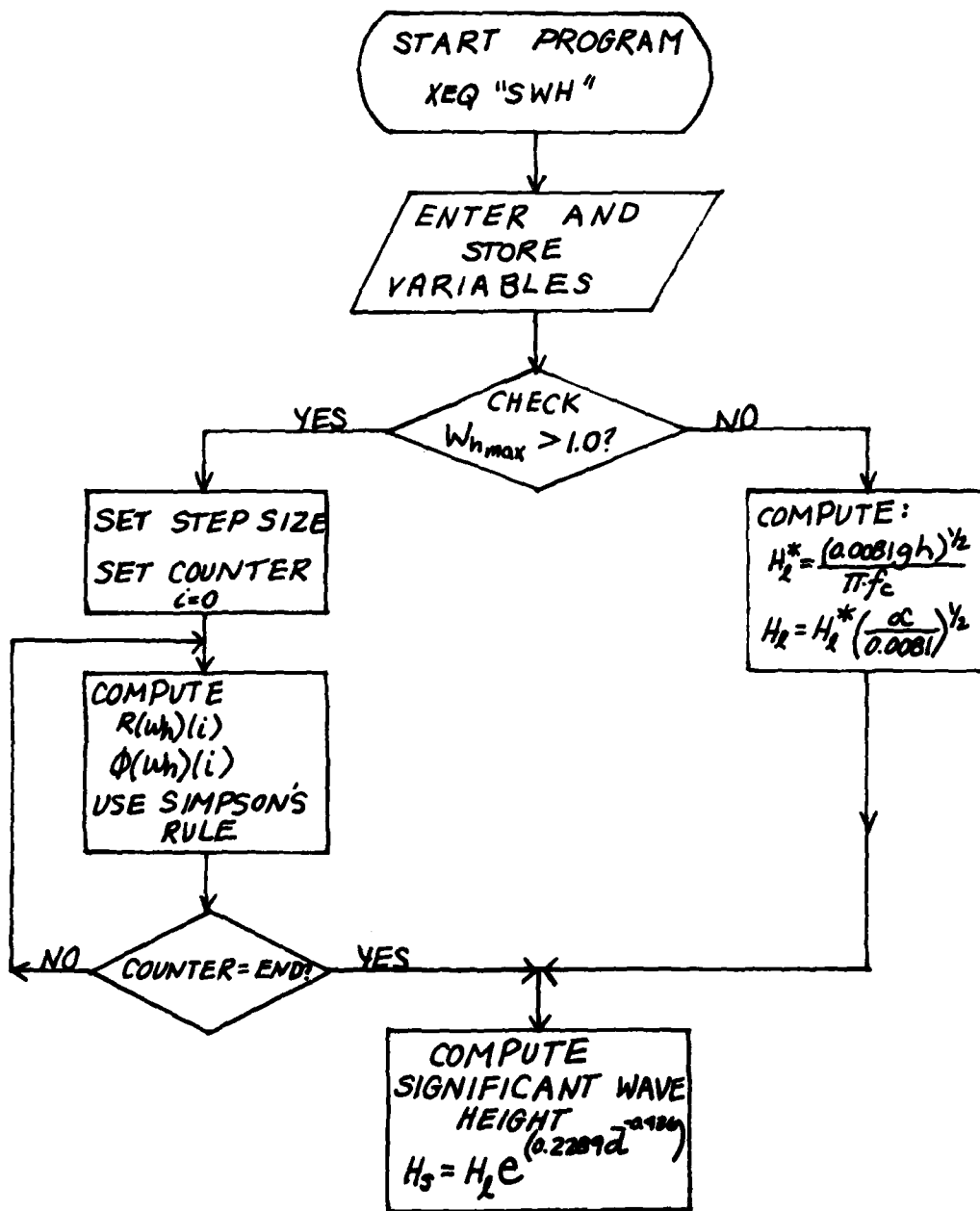
Thompson, E. F., and Vincent, C. L. "Significant Wave Height for Shallow Water Design," (submitted to ASCE for publication, June 1983).

Vincent, C. L. "A Method for Estimating Depth-Limited Wave Energy," Technical Aid No. 81-16, U. S. Army Corps of Engineers Coastal Engineering Research Center, November 1981.

Operating Limits and Warnings

107R-41CV-1

Program SWH Flowchart



107R-41CV-2

METHODOLOGY USED IN THE PROGRAM

Equations

Reference

Find $\omega_{h \max}$:

$$\omega_{h \max} = \omega_{\frac{h}{g}}^{\frac{1}{2}},$$

$$\omega = 2\pi f$$

$$\text{and } f = 2 \cdot fp$$

Equation (6): Vincent 1982

If $\omega_{h \max} \leq 1.0$

$$1. H_L^* = \frac{1}{\pi} (\omega gh)^{\frac{1}{2}} f_c^{-1}$$

Equation (16): Vincent 1982

$$2. H_L = H_L^* \left(\frac{\omega}{0.0081} \right)^{\frac{1}{2}}$$

Equation (15): Vincent 1982

$$3. H_s = H_L \exp \left(0.02289 \bar{d}^{-0.43642} \right)$$

Equation (5): Thompson and Vincent 1983

$$\text{Where } \bar{d} = \frac{h}{g T_p^2} = \frac{df^2}{g}$$

If $\omega_{h \max} > 1.0$

$$1. R(\omega_h) \tanh(\omega_h^2 R(\omega_h)) = 1$$

Equation (7): Vincent 1982

$$2. \phi(\omega_h) = R(\omega_h)^{-2} \left[1 + \frac{2\omega_h^2 R(\omega_h)}{\sinh(2\omega_h^2 R(\omega_h))} \right]^{-1}$$

Equation (5): Vincent 1982

$$3. E_h = \int_{0.8fp}^{2.0fp} \frac{\omega^2 f^{-5} \phi(\omega_h)}{(2\pi)^4} df$$

Equation (13): Vincent 1982

Simpson's Rule is used to numerically integrate Step 3

$$f(x)dx = \frac{h}{3} \left\{ y_0 + 4y_1 + 2y_2 + \dots + 4y_{i-1} + y_i \right\}$$

$$4. H_L^* = 4.0 (E_h)^{\frac{1}{2}}$$

Equation (14): Vincent 1982

$$5. H_L = H_L^* \left(\frac{\omega}{0.0081} \right)^{\frac{1}{2}}$$

Equation (15): Vincent 1982

$$6. H_s = H_L \exp \left(0.02289 \bar{d}^{-0.43642} \right)$$

Equation (5): Thompson and Vincent 1983

$$\bar{d} = \frac{h}{g T_p^2} = \frac{df^2}{g}$$

107R-41CV-3

User Instructions

107R-41CV: JONSWAP Depth-Limited Significant Wave Height

SIZE: 033

[illegible]

User Instructions

Example Problems

1. input: $d = 3\text{ft.} = 0.9144\text{m.}$
 $f_p = 0.0875$
 $\alpha = 0.0101$

SIGNIFICANT WAVE HT.
 ENGLISH UNITS
 DEPTH= 3.00000000 ***
 PEAK F= 0.08750000 ***
 ALPHA= 0.01010000 ***
 HS=7.712829318
 $H_L = 4.491602737$ ***

SIGNIFICANT WAVE HT.
 METRIC UNITS
 DEPTH= 0.914400000 ***
 PEAK F= 0.087500000 ***
 ALPHA= 0.010100000 ***
 HS=2.350066497
 $H_L = 1.368722437$ ***

2. input: $d = 30\text{ft.} = 9.144\text{m.}$
 $f_p = 0.0875$
 $\alpha = 0.0101$

SIGNIFICANT WAVE HT.
 ENGLISH UNITS
 DEPTH= 30.00000000 ***
 PEAK F= 0.087500000 ***
 ALPHA= 0.010100000 ***
 HS=15.90217827
 $H_L = 13.04655079$ ***

SIGNIFICANT WAVE HT.
 METRIC UNITS
 DEPTH= 9.144000000 ***
 PEAK F= 0.087500000 ***
 ALPHA= 0.010100000 ***
 HS=4.844781100
 $H_L = 3.974940560$ ***

3. input: $d = 10\text{ft.} = 3.048\text{m.}$
 $f_p = 0.1875$
 $\alpha = 0.02152$

SIGNIFICANT WAVE HT.
 ENGLISH UNITS
 DEPTH= 10.00000000 ***
 PEAK F= 0.187500000 ***
 ALPHA= 0.021520090 ***
 HS=6.004890523
 $H_L = 5.094608000$ ***

SIGNIFICANT WAVE HT.
 METRIC UNITS
 DEPTH= 3.048000000 ***
 PEAK F= 0.187500000 ***
 ALPHA= 0.021520090 ***
 HS=1.829502001
 $H_L = 1.552244259$ ***

4. input: $d = 15\text{ft.} = 4.572\text{m.}$
 $f_p = 0.1875$
 $\alpha = 0.02152$

SIGNIFICANT WAVE HT.
 ENGLISH UNITS
 DEPTH= 15.00000000 ***
 PEAK F= 0.187500000 ***
 ALPHA= 0.021520090 ***
 HS=7.060469425
 $H_L = 6.152105461$ ***

SIGNIFICANT WAVE HT.
 METRIC UNITS
 DEPTH= 4.572000000 ***
 PEAK F= 0.187500000 ***
 ALPHA= 0.021520090 ***
 HS=2.154519053
 $H_L = 1.872382756$ ***

Example problems 1 and 2 correspond to example problem #1 of Reference (3). Example problems 3 and 4 correspond to example problem #2 of Reference (3). Values of H_L (stored in R_{00}) have been printed out for comparison with the example problems of Reference (3). These program values differ from Reference (3) values because the integration limits in this program are from $0.8f_p$ to $2.0f_p$ and the limits used in the Reference (3) are from $0.9f_p$ to 1 Hz.

107R-41CV-5

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|-------------------|----------|----------|------|-----------|----------|---|
| 01 | LBL "SW" | | | 58 | RCL 07 | | |
| 02 | "SIGNIFICANT MAX" | | | 59 | RCL 06 | | |
| 03 | "E MT." | | | 60 | / | | |
| 04 | AVIEW | | | 61 | SORT | | |
| 05 | "E OR M" | | | 62 | RCL 03 | | |
| 06 | AOA | | | 63 | * | | |
| 07 | TONE 2 | | | 64 | STO 07 | | $W_{hmax} \rightarrow R_{07}$ |
| 08 | PROMPT | | | 65 | 1.0 | | |
| 09 | AOFF | | | 66 | X | | |
| 10 | ASTO Y | | | 67 | MMV | | $W_{hmax} > 1.0?$ |
| 11 | CLG | | | 68 | GTO 07 | | |
| 12 | "E" | | | 69 | 0.0081 | | |
| 13 | ASTO X | | | 70 | RCL 06 | | |
| 14 | CLA | | | 71 | * | | |
| 15 | X=Y? | | | 72 | RCL 01 | | |
| 16 | GTO 17 | | | 73 | * | | |
| 17 | "METRIC UNITS" | | | 74 | SORT | | |
| 18 | AVIEW | | | 75 | PI | | |
| 19 | 9.81 | | | 76 | / | | |
| 20 | GTO 18 | | | 77 | RCL 04 | | |
| 21 | LBL 17 | | | 78 | / | | $H_1^* = \frac{(0.0081gh)^{1/2}}{\pi f_c}$ |
| 22 | "ENGLISH UNITS" | | | 79 | RCL 05 | | |
| 23 | AVIEW | | | 80 | 0.0081 | | |
| 24 | 32.2 | | | 81 | / | | |
| 25 | LBL 18 | | | 82 | SORT | | |
| 26 | STO 06 | | | 83 | * | | |
| 27 | LBL 20 | | | 84 | STO 08 | | $H_2 = H_1^* \left(\frac{\alpha}{0.0081} \right)^{1/2} \rightarrow R_{08}$ |
| 28 | "DEPTH" | | | 85 | GTO 15 | | |
| 29 | TONE 3 | | | 86 | LBL 02 | | |
| 30 | PROMPT | | | 87 | RCL 02 | | |
| 31 | "DEPTH" | | | 88 | 2.0 | | |
| 32 | FS? 55 | | | 89 | * | | |
| 33 | XEQ 19 | | | 90 | STO 09 | | $2.0f_p \rightarrow R_{09}$ |
| 34 | STO 01 | | | 91 | RCL 04 | | |
| 35 | "PEAK F?" | | | 92 | - | | |
| 36 | TONE 4 | | | 93 | 4.0 | | |
| 37 | PROMPT | | | 94 | / | | |
| 38 | "PEAK F=" | | | 95 | STO 10 | | $dx \rightarrow R_{10}$ |
| 39 | FS? 55 | | | 96 | RCL 04 | | |
| 40 | XEQ 19 | | | 97 | STO 11 | | $f_c(i) \rightarrow R_{11}$ |
| 41 | STO 02 | | | 98 | 0.0 | | |
| 42 | 4 | | | 99 | STO 12 | | $counter \rightarrow R_{12}$ |
| 43 | * | | | 100 | LBL 04 | | |
| 44 | PI | | | 101 | 1.0 | | |
| 45 | * | | | 102 | RCL 12 | | |
| 46 | STO 03 | | | 103 | * | | |
| 47 | RCL 02 | | | 104 | STO 12 | | |
| 48 | 0.80 | | | 105 | RCL 01 | | |
| 49 | * | | | 106 | RCL 06 | | |
| 50 | STO 04 | | | 107 | / | | |
| 51 | "ALPHA" | | | 108 | SORT | | |
| 52 | TONE 5 | | | 109 | RCL 11 | | $counter(i) \rightarrow R_{12}$ |
| 53 | PROMPT | | | 110 | * | | |
| 54 | "ALPHA=" | | | 111 | 2 | | |
| 55 | FS? 55 | | | 112 | * | | |
| 56 | XEQ 19 | | | 113 | PI | | |
| 57 | STO 05 | | | 114 | * | | |
| | | | | 115 | X12 | | |

Simple
Solution
 $W_{hmax} < 1.0$

$$g \rightarrow R_{06}$$

$$d \rightarrow R_{01}$$

$$f_p \rightarrow R_{02}$$

$$W_{max} = 2\pi(2f_p) \rightarrow R_{05}$$

$$f_c \rightarrow R_{04}$$

$$\alpha \rightarrow R_{05}$$

$$W_{hmax} \rightarrow R_{07}$$

$$W_{hmax} > 1.0?$$

$$H_1^* = \frac{(0.0081gh)^{1/2}}{\pi f_c}$$

$$H_2 = H_1^* \left(\frac{\alpha}{0.0081} \right)^{1/2} \rightarrow R_{08}$$

$$2.0f_p \rightarrow R_{09}$$

$$dx \rightarrow R_{10}$$

$$f_c(i) \rightarrow R_{11}$$

$$counter \rightarrow R_{12}$$

$$counter(i) \rightarrow R_{12}$$

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|------------|----------|---|------|-----------|----------|--|
| 116 | STO 13 | | $[u_h(i)]^2 \rightarrow R_{13}$ | 172 | 5.0 | | |
| 117 | 0.0 | | | 173 | YTX | | |
| 118 | STO 21 | | | 174 | 2 | | |
| 119 | 1000.0 | | | 175 | P1 | | |
| 120 | STO 22 | | | 176 | * | | |
| 121 | 10.0 | | | 177 | 4.0 | | |
| 122 | STO 20 | | | 178 | YTX | | |
| 123 | LBL 05 | | | 179 | * | | |
| 124 | XEQ "CALC" | | | 180 | 1/X | | |
| 125 | 1.01 | | | 181 | 0.0081 | | |
| 126 | X<>Y | | | 182 | * | | |
| 127 | X<>Y | | ans. > 1.01 ? | 183 | RCL 06 | | |
| 128 | GTO 06 | | | 184 | Y+2 | | |
| 129 | GTO 07 | | | 185 | * | | |
| 130 | LBL 06 | | | 186 | RCL 16 | | |
| 131 | RCL 20 | | | 187 | * | | |
| 132 | STO 22 | | | 188 | STO 17 | | $\frac{(0.0081)q^2 \phi(u_h)}{f(i)^2 (2\pi)^4} \rightarrow R_{17}$ |
| 133 | RCL 21 | | | 189 | RCL 12 | | |
| 134 | + | | | 190 | 1.0 | | |
| 135 | 2 | | | 191 | X<>Y | | counter = 1.0? |
| 136 | / | | | 192 | X=Y? | | |
| 137 | GTO 05 | | | 193 | GTO 10 | | |
| 138 | LBL 07 | | | 194 | RCL 12 | | |
| 139 | 0.99 | | | 195 | 5.0 | | |
| 140 | X<>Y | | | 196 | X<>Y | | counter = 5.0? |
| 141 | X<>Y | | ans. > 0.99 ? | 197 | X=Y? | | |
| 142 | GTO 01 | | | 198 | GTO 11 | | |
| 143 | RCL 20 | | | 199 | RCL 12 | | |
| 144 | STO 21 | | | 200 | ENTER↑ | | |
| 145 | RCL 22 | | | 201 | 2 | | |
| 146 | + | | | 202 | MOD | | |
| 147 | 2 | | | 203 | X=0? | | |
| 148 | / | | | 204 | GTO 12 | | |
| 149 | GTO 05 | | | 205 | RCL 17 | | |
| 150 | LBL 08 | | | 206 | 2 | | |
| 151 | LASTX | | | 207 | * | | |
| 152 | STO 14 | | $R(u_h(i)) \rightarrow R_{14}$ | 208 | GTO 13 | | |
| 153 | RCL 14 | | | 209 | LBL 12 | | |
| 154 | RCL 13 | | | 210 | RCL 17 | | |
| 155 | * | | | 211 | 4 | | |
| 156 | 2 | | | 212 | * | | |
| 157 | * | | | 213 | GTO 13 | | |
| 158 | STO 15 | | $[2(u_h)^2 R(u_h)](i) \rightarrow R_{15}$ | 214 | LBL 13 | | |
| 159 | XEQ "SINH" | | | 215 | RCL 18 | | |
| 160 | 1/X | | | 216 | + | | |
| 161 | RCL 15 | | | 217 | STO 18 | | |
| 162 | * | | | 218 | RCL 11 | | |
| 163 | ! | | | 219 | RCL 10 | | |
| 164 | + | | | 220 | + | | $f(i)+dx \rightarrow R_{11}$ |
| 165 | 1/X | | | 221 | STO 11 | | |
| 166 | RCL 14 | | | 222 | GTO 04 | | |
| 167 | Y+2 | | | 223 | LBL 10 | | |
| 168 | 1/X | | | 224 | RCL 17 | | |
| 169 | * | | | 225 | STO 18 | | |
| 170 | STO 16 | | $\phi(u_h)(i) \rightarrow R_{16}$ | 226 | RCL 11 | | |
| 171 | RCL 11 | | | 227 | RCL 10 | | |
| | | | | 228 | + | | |

107R-41CV-7

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|------------|----------|----------|------|-----------|----------|----------|
| 229 | STO 11 | | | 285 | LBL 15 | | |
| 230 | GTO 04 | | | 286 | RCL 02 | | |
| 231 | LBL 11 | | | 287 | Y+Z | | |
| 232 | RCL 18 | | | 288 | RCL 01 | | |
| 233 | RCL 17 | | | 289 | * | | |
| 234 | + | | | 290 | RCL 06 | | |
| 235 | RCL 10 | | | 291 | / | | |
| 236 | * | | | 292 | -0.43642 | | |
| 237 | 3 | | | 293 | Y+X | | |
| 238 | / | | | 294 | 0.02289 | | |
| 239 | SORT | | | 295 | * | | |
| 240 | 4 | | | 296 | E+X | | |
| 241 | * | | | 297 | RCL 08 | | |
| 242 | RCL 05 | | | 298 | * | | |
| 243 | 0.0001 | | | 299 | MS= | | |
| 244 | / | | | 300 | ARCL X | | |
| 245 | SORT | | | 301 | AVIEW | | |
| 246 | * | | | 302 | TONE 6 | | |
| 247 | STO 08 | | | 303 | STOP | | |
| 248 | GTO 15 | | | 304 | GTO 20 | | |
| 249 | LBL "CALC" | | | 305 | END | | |
| 250 | STO 20 | | | | | | |
| 251 | RCL 13 | | | | | | |
| 252 | * | | | | | | |
| 253 | STO 30 | | | | | | |
| 254 | E+X | | | | | | |
| 255 | RCL 30 | | | | | | |
| 256 | CHS | | | | | | |
| 257 | E+X | | | | | | |
| 258 | + | | | | | | |
| 259 | STO 31 | | | | | | |
| 260 | RCL 30 | | | | | | |
| 261 | E+X | | | | | | |
| 262 | RCL 30 | | | | | | |
| 263 | CHS | | | | | | |
| 264 | E+X | | | | | | |
| 265 | - | | | | | | |
| 266 | RCL 31 | | | | | | |
| 267 | / | | | | | | |
| 268 | RCL 20 | | | | | | |
| 269 | * | | | | | | |
| 270 | RTN | | | | | | |
| 271 | LBL "SINH" | | | | | | |
| 272 | STO 32 | | | | | | |
| 273 | E+X | | | | | | |
| 274 | RCL 32 | | | | | | |
| 275 | CHS | | | | | | |
| 276 | E+X | | | | | | |
| 277 | - | | | | | | |
| 278 | 2 | | | | | | |
| 279 | | | | | | | |
| 280 | RTN | | | | | | |
| 281 | LBL 19 | | | | | | |
| 282 | P00 | | | | | | |
| 283 | P0X | | | | | | |
| 284 | RTN | | | | | | |

$$H_2 = H_2^* \left(\frac{\alpha}{0.0001} \right)^{1/2} \rightarrow R_{10}$$

$$\bar{d} = \frac{h f_p^2}{g}$$

$$H_3 = H_2 \exp(0.02289 \bar{d}^{-0.436})$$

REFERENCES

- Thompson, E. F., and Vincent, C. L. 1983. "Significant Wave Height for Shallow-Water Design," submitted for publication to The American Society of Civil Engineers.
- U. S. Army Engineer Waterways Experiment Station, Coastal Engineering Research Center (CERC). 1984. Shore Protection Manual, revised edition in preparation, U. S. Government Printing Office, Washington, D. C.
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- Walton, T. L., Birkemeier, W. A., and Weggel, J. R. 1982. "Hand-Held Calculator Algorithms for Coastal Engineering," Coastal Engineering Research Center Technical Aid 82-1, U. S. Army Engineer Waterways Experiment Station, Vicksburg, Miss.

APPENDIX A: BLANK PROGRAM FORMS

Program Description

| | | |
|--|--------------|-----------------|
| Program Title | | Date |
| Name | | |
| Address | | |
| City | State | Zip Code |
| Program Description, Equations, Variables, etc. | | |
| Operating Limits and Warnings | | |

User Instructions

[illegible]

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|-----------|----------|----------|------|-----------|----------|----------|
| 001 | | | | | | | |
| | | | | | | | |
| | | | | 060 | | | |
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| 010 | | | | | | | |
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[illegible]

